

# इंटरनेट

# मानक

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Mazdoor Kisan Shakti Sangathan

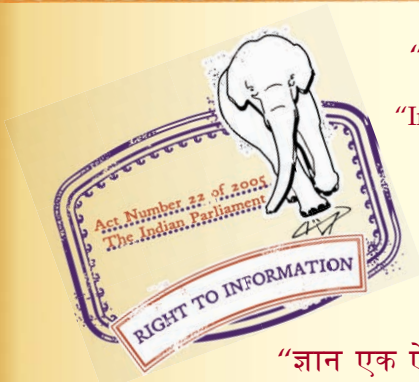
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SP 55 (1993): Design Aid for Anchorages for Spillway Piers, Training Walls and Divide Walls [WRD 9: Dams and Spillways]



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“ज्ञान एक ऐसा खजाना है जो कभी चुराया नहीं जा सकता है”

Bhartrhari—Nitiśatakam

“Knowledge is such a treasure which cannot be stolen”



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अधिप्लव पोत घाटों ट्रेनिंग दीवारों और विभाजन  
दीवारों के लिये लंगर कार्यों के डिजाइन एड

**DESIGN AID FOR ANCHORAGES FOR  
SPILLWAY PIERS, TRAINING WALLS AND  
DIVIDE WALLS**

UDC 627.231.8 : 72.011

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## FOREWORD

This special publication gives a method for design of anchorages for spillway piers, training walls and divide walls by computing stresses transferred to the base block from the piers/walls (*see* IS 12720 : 1993 'Structural design of spillway training walls and divide walls — Criteria' and IS 13551 : 1992 'Structural design of spillway crest and pier — Criteria' ) with the help of suitable tables.

For the purpose of deciding whether a particular requirement of this special publication, is complied with, the final value, observed or calculated expressing the result of a test analysis, should be rounded off in accordance with IS 2 : 1960 'Rules for rounding of numerical values (*revised*)'. The number of significant places retained in the rounded of value should be the same as that of the specified value in this special publication.

# DESIGN AID FOR ANCHORAGES FOR SPILLWAY PIERS, TRAINING WALLS AND DIVIDE WALLS

## 1 SCOPE

This Special Publication gives a method for the design of anchorages for spillway piers, training walls and divide walls with the help of tables.

## 2 METHOD ADOPTED FOR CALCULATION OF STRESSES

**2.1** Due to loading on the wall the stresses developed would be transferred to the base block and diffusion of stresses into the base block is of considerable importance for determination of depth of anchorage of reinforcing bars. The wall may be an end wall (see Fig. 1) or central wall (see Fig. 2). The diffusion of stresses would be in the quarter infinite block or end wall, whereas it would be in the semi-infinite block for the central wall.

**2.2** To obtain the stresses in the base block due to end wall, the following multiplication factors should be worked out:

$$\frac{F}{b}, \frac{P}{b} \quad \text{and} \quad \frac{M}{b^2}$$

where

$F$  = shear force at the base of the wall,

$P$  = normal force,

$M$  = moment at the base of the wall, and

$b$  = base width of the wall.

The horizontal stress  $\sigma_x$ , the vertical stress  $\sigma_y$  and shear stress  $\tau_{xy}$  due to unit value of shear force  $F$ , moment  $M$ , and normal force  $P$ , are given in the Tables 1, 2 and 3 respectively for different values of

$\frac{x}{b}$  and  $\frac{y}{b}$  where  $x$  and  $y$  are the distances along horizontal and vertical axis from the origin as shown in Fig. 1.

**2.3** To obtain the stresses in the base block due to central wall, the following multiplication factors should be worked out:

$$\frac{F}{b}, \frac{P}{b} \quad \text{and} \quad \frac{6M}{b^2}$$

The stresses due to unit value of shear force  $F$ , moment  $M$  and normal force  $P$  are given in the Tables 4, 5 and 6 respectively for different values of

$\frac{x}{b}$  and  $\frac{y}{b}$  where  $x$  and  $y$  are the distances along horizontal and vertical axis from the origin as shown in Fig. 2.

**2.4** The actual horizontal and vertical stress should be obtained by multiplying the unit values given in the tables with corresponding multiplication factor.

**2.5** For horizontal anchorage,  $\alpha x$  distribution is plotted at different vertical sections and the total tensile force is calculated at each of these sections. The horizontal anchorage steel is provided for the maximum tensile force obtained at these vertical sections.

**2.6** The vertical stresses in the base block would diminish as the depth increases. Hence, the vertical reinforcement in the wall may be continued up to the depth where the tensile stresses developed are within permissible limits.

**2.7** Computations based on these tables for design of anchorages for a divide wall resting directly over the foundation rock are given in Annex A.

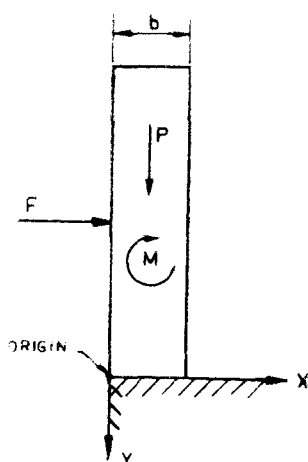


FIG. 1 END WALL

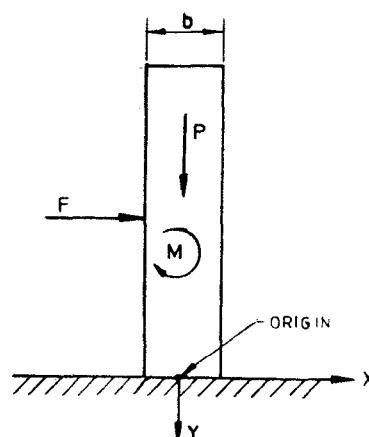
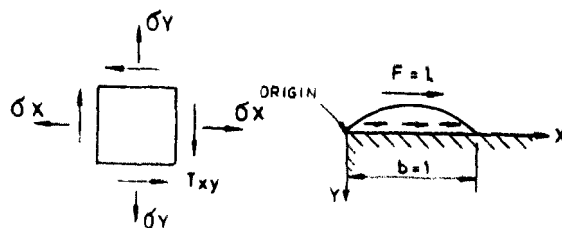


FIG. 2 CENTRAL WALL

**Table 1 Stresses in End Wall Due to Unit Shear Force**  
( Clause 2.2 )



$x/b \backslash y/b$	0.00	0.25	0.50	0.75	1.00	1.25	1.50	1.75	2.00
0.00	0.00 0.00 0.00	0.19 0.00 1.13	1.50 0.00 1.50	2.80 0.00 1.13	2.87 0.00 0.00	1.97 0.00 0.00	1.53 0.00 0.00	1.26 0.00 0.00	1.07 0.00 0.00
0.25	0.00 -1.12 0.00	0.32 -0.51 0.46	0.96 0.00 0.71	1.35 0.27 0.58	1.47 0.28 0.46	1.37 0.12 0.35	1.20 0.06 0.25	1.07 0.03 0.18	0.96 0.03 0.13
0.50	0.00 -1.28 0.00	0.13 -0.64 0.06	0.45 0.00 0.23	0.64 0.92 0.34	0.80 0.32 0.42	0.87 0.22 0.39	0.88 0.15 -0.32	0.84 0.09 0.26	0.80 0.07 0.21
0.75	0.00 -1.25 0.00	0.02 -0.77 -0.06	0.10 -0.20 0.02	0.25 0.13 0.16	0.40 0.26 0.27	0.52 0.24 0.31	0.59 0.19 0.31	0.62 0.14 0.27	0.62 0.11 0.24
1.00	0.00 -1.08 0.00	-0.01 -0.71 -0.09	0.02 -0.31 -0.06	0.08 0.02 0.04	0.18 0.17 0.15	0.29 0.21 0.22	0.38 0.19 0.24	0.44 0.16 0.25	0.46 0.13 0.23
1.25	0.00 -0.96 0.00	0.00 -0.67 -0.08	0.00 -0.35 -0.09	0.03 -0.08 -0.03	0.09 0.08 0.06	0.16 0.15 0.13	0.23 0.18 0.18	0.29 0.16 0.20	0.32 0.14 0.20
1.50	0.00 -0.87 0.00	0.00 -0.61 -0.08	-0.01 -0.37 -0.10	0.00 -0.15 -0.06	0.04 0.00 0.00	0.09 0.09 0.07	0.14 0.14 0.12	0.19 0.14 0.15	0.23 0.14 0.16
1.75	0.00 -0.77 0.00	-0.01 -0.57 -0.07	-0.02 -0.37 -0.09	-0.01 -0.19 -0.08	0.01 0.05 -0.03	0.03 0.04 0.02	0.08 0.10 0.07	0.12 0.11 0.11	0.15 0.12 0.13
2.00	0.00 -0.67 0.00	-0.01 -0.53 -0.07	-0.02 -0.37 -0.08	-0.02 -0.22 -0.08	-0.01 -0.09 -0.05	0.01 -0.01 0.00	0.03 0.06 0.03	0.07 0.08 0.08	0.10 0.09 0.10

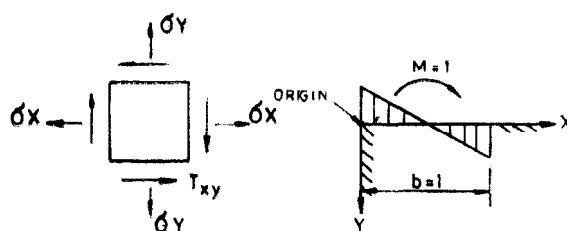
## NOTES

1 The order of listing of the stresses  $\sigma_x$ ,  $\sigma_y$ ,  $\tau_{xy}$  is  $\begin{Bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{Bmatrix}$

2 The negative sign indicates tension and positive sign indicates compression.

**Table 2 Stresses in End Wall Due to Unit Moment**

( Clause 2.2 )



$x/b \backslash y/b$	0.00	0.25	0.50	0.75	1.00	1.25	1.50	1.75	2.00
0.00	0.00 -0.60 0.00	0.38 -3.00 0.00	1.79 0.00 0.00	3.84 3.00 0.00	3.33 6.00 0.00	1.00 0.00 0.00	0.60 0.00 0.00	0.50 0.00 0.00	0.50 0.00 0.00
0.25	0.00 -5.10 0.00	0.38 -2.69 -0.73	0.83 0.13 -0.91	0.90 2.37 -0.43	0.91 1.50 0.50	1.00 0.38 0.28	0.94 0.13 0.27	0.64 0.09 0.22	0.45 0.04 0.13
0.50	0.00 -3.71 0.00	-0.10 -2.24 -0.94	-0.19 -0.19 -0.97	-0.20 0.14 -0.42	0.07 1.34 0.37	0.37 0.69 0.60	0.43 0.27 0.38	0.39 0.12 0.26	0.40 0.08 0.21
0.75	0.00 -2.43 0.00	-0.26 -1.86 -0.72	-0.45 -0.38 -0.90	-0.51 0.77 -0.45	-0.30 0.97 0.03	0.02 0.73 0.48	0.17 0.37 0.34	0.24 0.20 0.27	0.19 0.14 0.22
1.00	0.00 -1.66 0.00	-0.12 -1.34 -0.50	-0.32 -0.51 -0.70	-0.47 0.32 -0.53	-0.37 0.53 -0.13	-0.27 0.50 0.22	-0.04 0.40 0.24	0.01 0.18 0.20	0.06 0.18 0.19
1.25	0.00 -1.28 0.00	-0.01 -0.94 -0.35	-0.18 -0.49 -0.55	-0.35 0.10 -0.34	-0.38 0.33 -0.12	-0.28 0.38 0.03	-0.20 0.29 0.09	-0.10 0.24 0.13	-0.09 0.13 0.11
1.50	0.00 -0.89 0.00	-0.07 -0.69 -0.27	-0.15 -0.37 -0.38	-0.31 -0.11 -0.33	-0.20 0.16 -0.19	-0.29 0.20 -0.10	-0.20 0.22 0.00	-0.10 0.15 0.03	-0.09 0.18 0.09
1.75	0.00 -0.65 0.00	0.02 -0.52 -0.16	0.01 -0.33 -0.26	-0.14 -0.18 -0.27	-0.30 -0.07 -0.21	-0.30 0.10 -0.14	-0.27 0.21 -0.09	-0.16 0.16 0.00	-0.12 0.15 0.04
2.00	0.00 -0.50 0.00	-0.02 -0.46 -0.12	-0.08 -0.34 -0.20	-0.14 -0.20 -0.22	-0.18 -0.06 -0.19	-0.19 -0.01 -0.17	-0.18 0.09 -0.09	-0.16 0.12 -0.04	-0.12 0.12 0.00

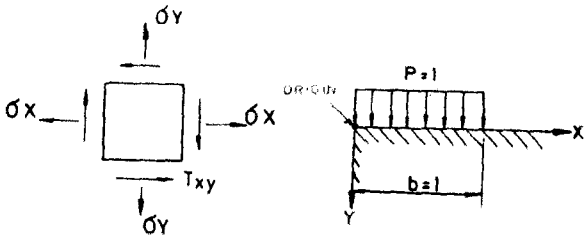
## NOTES

1 The order of listing of the stresses  $\sigma_x$ ,  $\sigma_y$ ,  $\tau_{xy}$  is  $\begin{cases} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{cases}$

2 The negative sign indicates tension and positive sign indicates compression.



Table 3 Stresses in End Wall Due to Unit Normal Force  
( Clause 2.2 )



$x/b \backslash y/b$	0.00	0.25	0.50	0.75	1.00	1.25	1.50	1.75	2.00
0.00	0.00 1.00 0.00	0.03 1.00 0.00	0.07 1.00 0.00	0.13 1.00 0.00	-0.25 1.00 0.00	-0.57 0.00 0.00	-0.46 0.00 0.00	-0.45 0.00 0.00	-0.43 0.00 0.00
0.25	0.00 1.00 0.00	0.03 1.10 0.00	0.03 0.93 0.02	0.06 0.90 0.08	-0.06 0.56 0.13	-0.19 0.04 0.08	-0.26 0.02 0.03	-0.29 0.06 0.00	-0.30 0.00 -0.01
0.50	0.00 1.10 0.00	0.02 0.96 -0.02	0.01 0.90 0.05	0.00 0.88 0.10	-0.03 0.43 0.24	-0.09 0.14 0.16	-0.14 0.07 0.08	-0.17 0.03 0.03	-0.20 0.02 0.01
0.75	0.00 1.15 0.00	0.00 0.83 -0.02	-0.06 0.85 0.06	-0.06 0.77 0.17	-0.08 0.45 0.22	-0.05 0.23 0.18	-0.07 0.13 0.11	-0.09 0.07 0.06	-0.12 0.04 0.03
1.00	0.00 1.28 0.00	-0.06 0.83 0.03	-0.09 0.74 0.07	-0.04 0.61 0.16	-0.03 0.44 0.19	-0.03 0.29 0.17	-0.03 0.18 0.12	0.04 0.11 -0.08	-0.06 0.07 0.05
1.25	0.00 1.07 0.00	-0.07 0.88 0.07	-0.06 0.74 0.104	-0.036 0.59 0.13	-0.02 0.45 0.17	-0.004 0.32 0.16	0.00 0.21 0.13	-0.01 0.14 0.10	-0.02 0.09 0.07
1.50	0.00 0.98 0.00	0.00 0.83 0.07	-0.003 0.70 0.11	-0.01 0.57 0.14	0.01 0.44 0.15	0.02 0.33 0.15	0.02 0.28 0.13	0.01 0.17 0.11	0.01 0.12 0.08
1.75	0.00 0.90 0.00	0.00 0.75 0.07	0.01 0.66 0.11	0.02 0.55 0.13	-0.02 0.44 0.15	0.03 0.34 0.14	0.03 0.26 0.13	0.03 0.19 0.11	0.02 0.14 0.09
2.00	0.00 0.82 0.00	0.00 0.73 0.06	0.01 0.63 0.10	0.02 0.53 -0.13	0.03 0.44 0.14	0.035 0.35 0.14	0.04 0.27 0.13	0.04 0.21 0.11	0.04 0.16 0.10

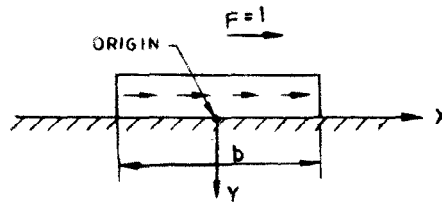
NOTES

1 The order of listing of the stresses  $\sigma_x$ ,  $\sigma_y$ ,  $\tau_{xy}$  is  $\begin{cases} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{cases}$

2 The negative sign indicates tension and positive sign indicates compression.

Table 4 Stresses in Central Wall Due to Unit Shear Force

(Clause 2.3)

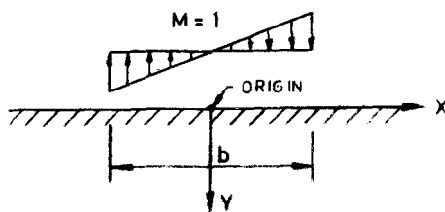


$x/b \backslash y/b$	0.00	0.25	0.50	0.75	1.00	1.25	1.50	1.75	2.00	Stresses
0.00	0.000 0	0.699 4	2.925 0*	1.024 6	0.699 4	0.539 4	0.441 3	0.374 2	0.325 2	$\sigma_x$
	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	$\sigma_y$
	-1.000 0	-1.000 0	-1.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	$\tau_{xy}$
0.25	0.000 0	0.385 0	0.602 3	0.669 5	0.582 0	0.486 8	0.413 1	0.357 3	0.314 2	$\sigma_x$
	0.000 0	0.127 3	0.299 6	0.146 9	0.055 1	0.025 5	0.013 8	0.008 4	0.005 5	$\sigma_y$
	-0.450 2	-0.392 9	-0.347 1	-0.285 1	-0.170 7	-0.108 2	-0.074 1	-0.053 9	-0.040 9	$\tau_{xy}$
0.50	0.000 0	0.147 4	0.257 7	0.348 8	0.385 0	0.373 4	0.344 6	0.313 4	0.284 6	$\sigma_x$
	0.000 0	0.156 7	0.254 6	0.210 7	0.127 3	0.073 9	0.044 9	0.028 9	0.019 6	$\sigma_y$
	-0.181 7	-0.186 2	-0.225 1	-0.248 9	-0.211 2	-0.161 4	-0.122 0	-0.093 9	-0.073 9	$\tau_{xy}$
0.75	0.000 0	0.059 8	0.121 5	0.187 3	0.238 5	0.262 7	0.265 7	0.257 4	0.244 2	$\sigma_x$
	0.000 0	0.127 3	0.203 7	0.202 2	0.156 7	0.109 8	0.075 3	0.052 4	0.037 4	$\sigma_y$
	-0.080 5	-0.097 8	-0.142 4	-0.180 6	-0.184 8	-0.165 0	-0.138 8	-0.114 5	-0.094 5	$\tau_{xy}$
1.00	0.000 0	0.026 9	0.061 5	0.101 9	0.147 4	0.178 8	0.196 2	0.202 4	0.201 4	$\sigma_x$
	0.000 0	0.095 9	0.159 2	0.175 4	0.156 7	0.125 4	0.095 5	0.071 7	0.054 0	$\sigma_y$
	-0.040 5	-0.055 1	-0.090 8	-0.126 9	-0.145 7	-0.145 6	-0.134 2	-0.118 8	-0.103 2	$\tau_{xy}$
1.25	0.000 0	0.013 4	0.033 2	0.061 2	0.092 7	0.121 0	0.142 0	0.155 1	0.161 6	$\sigma_x$
	0.000 0	0.072 0	0.124 2	0.146 9	0.144 0	0.126 5	0.104 7	0.084 1	0.066 8	$\sigma_y$
	-0.022 7	-0.033 2	-0.059 5	-0.089 2	-0.111 0	-0.120 4	-0.119 6	-0.112 6	-0.102 8	$\tau_{xy}$
1.50	0.000 0	0.007 2	0.019 1	0.037 3	0.059 8	0.082 6	0.102 4	0.117 4	0.127 5	$\sigma_x$
	0.000 0	0.055 1	0.097 9	0.121 9	0.127 3	0.119 8	0.105 8	0.089 9	0.074 9	$\sigma_y$
	-0.013 8	-0.021 2	-0.040 3	-0.063 6	-0.083 9	-0.096 9	-0.102 1	-0.101 3	-0.096 7	$\tau_{xy}$
1.75	0.000 0	-0.004 2	0.011 6	0.023 6	0.039 6	0.057 2	0.074 1	0.088 6	0.099 8	$\sigma_x$
	0.000 0	0.043 0	0.078 4	0.010 12	0.110 8	0.109 8	0.101 9	0.090 8	0.078 8	$\sigma_y$
	-0.009 0	-0.014 2	-0.028 1	-0.046 3	-0.063 8	-0.077 2	-0.085 3	0.088 4	-0.087 8	$\tau_{xy}$
2.00	0.000 0	0.002 6	0.007 4	0.015 5	0.026 9	0.040 3	0.054 1	0.067 0	0.078 0	$\sigma_x$
	0.000 0	0.034 3	0.063 7	0.084 5	0.095 9	0.098 8	0.095 5	0.088 4	0.079 5	$\sigma_y$
	-0.006 2	-0.010 0	-0.020 3	-0.034 3	-0.049 0	-0.061 5	-0.070 6	-0.075 9	-0.077 9	$\tau_{xy}$

\* at  $x/b = 0.49$  and  $y/b = 0$ 

Note — Positive sign indicates compressive stresses and negative sign indicates tensile stresses.

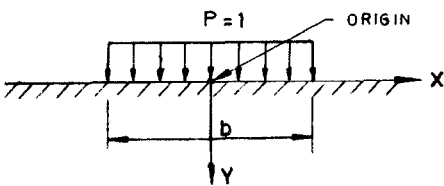
**Table 5 Stresses in Central Wall Due to Unit Moment**  
( Clause 2.3 )



$x/b$ $y/b$	0.00	0.25	0.50	0.75	1.00	1.25	1.50	1.75	2.00	Stresses
0.00	0.000 0	+0.500 0	1.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	$\sigma_x$
	0.000 0	+0.500 0	1.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	$\sigma_y$
	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	$\tau_{xy}$
0.25	0.000 0	0.004 0	0.046 0	0.092 9	0.050 4	0.027 0	0.015 8	0.010 0	0.006 7	$\sigma_x$
	0.000 0	0.387 5	0.347 1	0.060 4	0.011 1	0.003 1	0.001 1	0.000 5	0.000 2	$\sigma_y$
	0.225 1	0.132 8	-0.126 0	-0.077 8	-0.024 8	-0.009 6	-0.004 4	-0.002 3	-0.001 3	$\tau_{xy}$
0.50	0.000 0	-0.054 4	-0.032 6	0.024 5	0.037 5	0.030 1	0.021 5	0.015 2	0.010 9	$\sigma_x$
	0.000 0	0.210 6	0.225 1	0.109 9	0.040 5	0.015 5	0.006 6	0.003 1	0.001 6	$\sigma_y$
	0.181 7	0.107 8	-0.029 6	-0.067 3	-0.043 4	-0.023 4	-0.012 8	-0.007 4	-0.004 5	$\tau_{xy}$
0.75	0.000 0	-0.040 8	-0.039 8	-0.010 0	-0.011 9	0.018 5	0.017 7	0.014 8	0.011 8	$\sigma_x$
	0.000 0	0.112 5	0.142 4	0.102 4	0.056 3	0.028 4	0.014 5	0.007 7	0.004 3	$\sigma_y$
	0.120 8	0.083 0	0.009 8	-0.032 4	-0.036 2	-0.026 9	-0.017 9	-0.011 7	-0.007 7	$\tau_{xy}$
1.00	0.000 0	-0.026 2	-0.032 1	-0.019 4	-0.003 6	-0.006 4	0.010 4	0.011 0	0.010 1	$\sigma_x$
	0.000 0	0.063 5	0.090 8	0.080 7	0.056 3	0.034 9	0.020 8	0.012 4	0.007 5	$\sigma_y$
	0.081 0	0.062 3	0.022 5	0.009 3	-0.022 1	-0.022 2	-0.018 0	-0.013 4	0.009 8	$\tau_{xy}$
1.25	0.000 0	-0.016 8	-0.023 6	-0.019 3	0.009 9	-0.001 5	0.003 8	0.006 4	0.007 2	$\sigma_x$
	0.000 0	0.038 2	0.059 5	0.060 4	0.049 2	0.035 4	0.023 9	0.015 8	0.010 4	$\sigma_y$
	0.056 8	0.047 0	0.024 5	0.002 7	-0.010 5	-0.015 2	-0.015 0	-0.012 8	-0.010 2	$\tau_{xy}$
1.50	0.000 0	-0.011 1	-0.017 1	-0.016 4	-0.011 5	-0.005 6	-0.000 8	0.002 4	0.004 2	$\sigma_x$
	0.000 0	0.024 4	0.040 3	0.044 7	0.040 5	0.032 5	0.024 3	0.017 5	0.012 3	$\sigma_y$
	0.041 5	0.036 1	0.022 8	0.008 2	-0.002 9	-0.008 9	-0.011 0	-0.010 7	-0.009 5	$\tau_{xy}$
1.75	0.000 0	-0.007 6	-0.012 4	-0.013 3	-0.010 9	-0.007 2	-0.003 4	-0.000 4	-0.001 6	$\sigma_x$
	0.000 0	0.016 3	0.028 1	0.033 3	0.032 6	0.028 4	0.023 0	0.017 7	0.013 3	$\sigma_y$
	0.031 5	0.028 3	0.020 1	0.010 2	0.001 6	-0.004 2	0.007 2	-0.008 2	-0.008 0	$\tau_{xy}$
2.00	0.000 0	-0.005 4	-0.009 2	-0.010 5	-0.009 6	-0.007 4	-0.004 7	-0.002 2	-0.000 2	$\sigma_x$
	0.000 0	0.011 4	0.020 3	0.025 1	0.026 0	0.024 1	0.020 8	0.017 0	0.013 5	$\sigma_y$
	0.024 7	0.022 7	0.017 4	0.010 6	0.004 1	-0.000 9	-0.004 1	-0.005 8	-0.006 4	$\tau_{xy}$

NOTE — Positive sign indicates compressive stresses and negative sign indicates tensile stresses.

Table 6 Stresses in Central Wall Due to Unit Normal Force  
(Clause 2.3)



$x/b$ $y/b$	0.00	0.25	0.50	0.75	1.00	1.25	1.50	1.75	2.00	Stresses
0.00	+1.000 0	+1.000 0	1.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	$\sigma_x$
	+1.000 0	+1.000 0	1.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	$\sigma_y$
	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	0.000 0	$\tau_{xy}$
0.25	0.450 2	0.392 9	0.347 1	0.285 1	0.170 7	0.108 2	0.074 1	0.053 9	0.040 9	$\sigma_x$
	0.959 5	0.902 2	0.496 9	0.089 2	0.019 3	0.006 3	0.002 7	0.001 3	0.000 7	$\sigma_y$
	0.000 0	-0.127 3	-0.299 6	-0.146 9	-0.055 1	-0.025 5	-0.013 8	-0.008 4	-0.005 5	$\tau_{xy}$
0.50	0.181 7	0.186 2	0.225 1	0.248 9	0.211 2	0.161 4	0.122 0	0.093 9	0.073 9	$\sigma_x$
	0.818 3	0.734 7	0.479 7	0.213 7	0.083 9	0.035 8	0.017 2	0.009 2	0.005 3	$\sigma_y$
	0.000 0	-0.156 7	-0.254 6	-0.210 7	-0.127 3	-0.073 9	-0.044 9	-0.028 9	-0.019 6	$\tau_{xy}$
0.75	0.080 5	0.097 8	0.142 4	0.180 6	0.184 8	0.165 0	0.138 8	0.114 5	0.094 5	$\sigma_x$
	0.668 2	0.607 1	0.448 0	0.270 5	0.145 7	0.077 2	0.042 5	0.021 7	0.015 1	$\sigma_y$
	0.000 0	-0.127 3	-0.203 7	-0.202 2	-0.156 7	-0.109 8	-0.075 3	-0.052 4	-0.037 4	$\tau_{xy}$
1.00	0.040 5	0.055 1	0.090 8	0.126 9	0.145 7	0.145 6	0.134 2	0.118 8	0.103 2	$\sigma_x$
	0.549 8	0.510 5	0.409 2	0.287 6	0.184 8	0.114 2	0.070 6	0.044 5	0.028 9	$\sigma_y$
	0.000 0	-0.095 9	-0.159 2	-0.175 4	-0.156 7	-0.125 4	-0.095 5	-0.071 7	-0.054 0	$\tau_{xy}$
1.25	0.022 7	0.033 2	0.059 5	0.089 2	0.111 0	0.120 4	0.119 6	0.112 6	0.102 8	$\sigma_x$
	0.461 8	0.436 5	0.370 0	0.285 1	0.204 5	0.140 7	0.095 2	0.064 6	0.044 3	$\sigma_y$
	0.000 0	-0.072 0	-0.124 2	-0.146 9	-0.144 0	-0.126 5	-0.104 7	-0.084 1	-0.066 8	$\tau_{xy}$
1.50	0.013 8	0.021 2	0.040 3	0.063 6	0.083 9	0.096 9	0.102 1	0.101 3	0.096 7	$\sigma_x$
	0.395 8	0.379 1	0.334 1	0.273 5	0.211 2	0.156 8	0.113 9	0.082 1	0.059 3	$\sigma_y$
	0.000 0	-0.055 1	-0.097 9	-0.121 9	-0.127 3	-0.119 8	-0.105 8	-0.089 9	-0.074 9	$\tau_{xy}$
1.75	0.009 0	0.014 2	0.028 1	0.046 3	0.063 8	0.077 2	0.085 3	0.088 4	0.087 8	$\sigma_x$
	0.345 3	0.333 9	0.302 4	0.258 3	0.210 2	0.165 0	0.126 6	0.095 9	0.072 3	$\sigma_y$
	0.000 0	-0.043 0	-0.078 4	-0.101 2	-0.110 8	-0.109 8	-0.101 9	-0.090 8	-0.078 8	$\tau_{xy}$
2.00	0.006 2	0.010 0	0.020 3	0.034 3	0.049 0	0.061 5	0.070 6	0.075 9	0.077 9	$\sigma_x$
	0.305 8	0.297 6	0.274 6	0.242 1	0.204 7	0.167 7	0.134 2	0.105 9	0.082 9	$\sigma_y$
	0.000 0	-0.034 3	-0.063 7	-0.084 5	-0.095 9	-0.098 8	-0.095 5	-0.088 4	-0.079 5	$\tau_{xy}$

NOTE — Positive sign indicates compressive stresses and negative sign indicates tensile stresses.

## ANNEX A

( Clause 2.7 )

COMPUTATIONS FOR DESIGN OF ANCHORAGE REINFORCEMENT  
FOR A DIVIDE WALL ( see Fig. 3 )

Given :

1. Base width of wall = 2.5 m
2. Direct load per m run = 72 t
3. Shear force per metre run = 50 t
4. Bending moment per metre run  
= 166.667 t.m
5. Vertical reinforcement in wall on either face for direct load and moment = 25 mm deformed bars conforming to IS 1786 : 1985 @ 140 mm c/c
6. Concrete mix used = M 20
7. Permissible tensile stress in steel = 80% of  $2.300 \text{ t/cm}^2 = 1.84 \text{ t/cm}^2$
8. Allowable tensile stress in concrete = 1% of compressive strength of concrete =  $0.01 \times 2000 = 20 \text{ t/m}^2$
9. Allowable tensile stress of fresh rock =  $20 \text{ t/m}^2$  (assumed same as concrete in this example. For permissible stresses relevant Indian Standard be referred to)
10. The anchorages for the divide wall are to be designed for loading on one side and with no water on other side and vice/versa.

As there is concrete slab on both sides of the wall, therefore, semi-plate infinite theory (see 2.3) should be used to calculate horizontal anchorage and the depth up to which the vertical reinforcement bars should be taken to.

Here

Direct load per metre run

$$P = 72 \text{ t.}$$

Shear force per metre run

$$F = -50 \text{ t.}$$

Bending moment per metre run

$$M = -166.667 \text{ t.m}$$

## Multiplication Factors

$$\frac{P}{b} = \frac{72}{2.5} = 28.80 \text{ t/m}^2$$

$$\frac{E}{b} = \frac{-50}{2.5} = -20.0 \text{ t/m}^2$$

$$\frac{6M}{b^2} = \frac{-6 \times 166.667}{(2.5)^2} = -160.00 \text{ t/m}^2$$

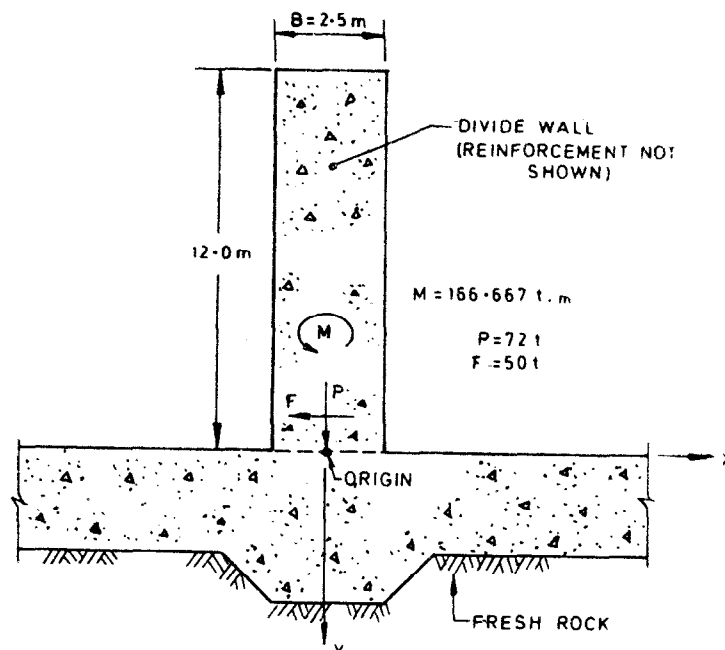


FIG. 3 DESIGN OF A DIVIDE WALL

Total horizontal and vertical stresses at different points calculated on the basis of different tables are indicated in Table 7 and 8 respectively.

### Design of Horizontal Anchorage

For design of horizontal anchorage horizontal stresses on vertical planes should be considered. Table 7 (indicating the value of  $\alpha x$ ) is referred to:

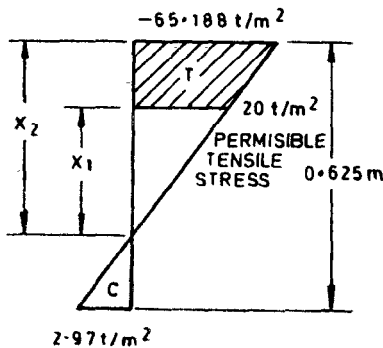
i) At  $x/b = 0.25$

Here

$$\frac{65.188}{x_2} = \frac{2.97}{0.625 - x_2}$$

$$\text{or } x_2 = \frac{65.188 \times 0.625}{65.188 + 2.97}$$

$$= 0.598 \text{ m}$$



Also

$$\frac{65.188}{0.598} = \frac{20}{x_1} \quad \text{or } x_1 = 0.18 \text{ m}$$

Total tensile force (hatched area)

$$= \frac{(65.188 + 20)}{2} \times (0.598 - 0.18)$$

$$= 17.8 \text{ t/m-run}$$

ii) At  $x/b = 0.50$

Here

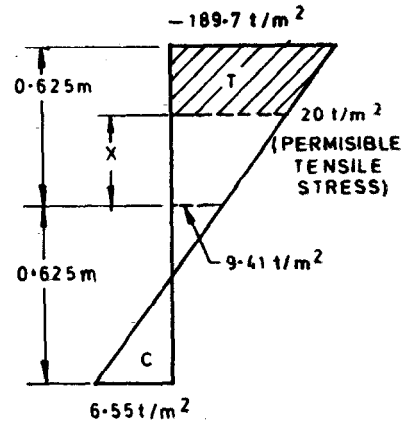
$$\frac{(189.70 - 9.41)}{0.625} = \frac{(20 - 9.41)}{x}$$

$$\text{or } x = 0.0367 \text{ m}$$

Total tensile force (hatched area)

$$= \frac{(189.7 + 20)}{2} \times (0.625 - 0.0367)$$

$$= 61.68 \text{ t/m-run}$$



iii) At  $x/b = 0.75$

From Table 7 it may be seen that the maximum tensile stress at this section is  $20.4 \text{ t/m}^2$  which is approximately equal to the permissible tensile stress  $20 \text{ t/m}^2$ , hence no reinforcement is required at this section.

From the above it is seen that maximum horizontal tensile force is:

$$= 61.68 \text{ t/m-run}$$

Area of steel required

$$= \frac{61.88}{1.84} = 33.5 \text{ cm}^2$$

Provided 25 mm deformed steel bars @ 140 mm c/c

The length on either side of the divide wall up to which horizontal anchorage reinforcement to be provided is determined in the following manner :

i) At  $x/b = 0.5$  (face of the wall)

$$\text{Anchorage length required} = 45 d = 45 \times 25 = 1125 \text{ mm}$$

$$= 1.125 \text{ m from the face of the wall.}$$

ii) At  $x/b = 0.75$  maximum tensile stress is equal to  $20.49 \text{ t/m}^2$ , which is very close to the tensile stress of  $20 \text{ t/m}^2$  for the mix used. The steel rods are not under tension here.

Reinforcement is required up to a length equal to  $12 d$  beyond this point, that is,  $12 \times 25 = 300 \text{ mm} = 0.30 \text{ m}$  or  $0.625 + 0.30 = 0.925 \text{ m}$  from the face of the wall. Hence provide horizontal anchorage up to 1.125 m (1.20 m say) from the face of the wall.

### Design of Vertical Anchorage

For design of the depth of vertical anchorage Table 8 should be used.

It is seen that for a permissible tensile stress of  $20 \text{ t/m}^2$ , a depth of  $0.75 b$  (width of divide wall) should be sufficient (In table 8 at  $x/b = 0.5$  and  $y/b = 0.75$ ;  $\sigma_y$  is only  $13.9 \text{ t/m}^2$  tensile). However,

vertical anchorage may be provided for a minimum depth equal to thickness of the divide wall, that is,  $2.5 \text{ m}$ .

Reinforcement details are shown in Fig. 4.

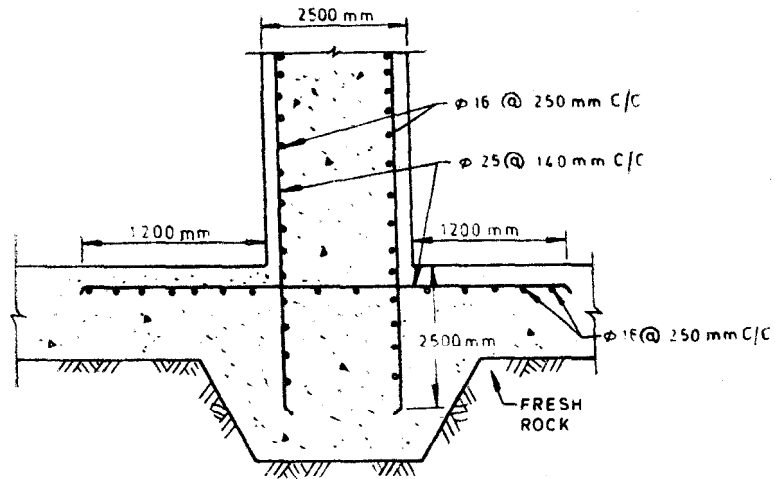


FIG. 4 TYPICAL REINFORCEMENT DETAILS OF ANCHORAGE

Table 7 Computation of Horizontal Stress ( $\sigma_x$ ) at Different Points

(Annex A)

$$\frac{F}{b} = \frac{-50}{2.5} = -20.0 \text{ t/m}^2$$

$$\frac{P}{b} = \frac{72}{2.5} = 28.8 \text{ t/m}^2$$

$$\frac{6M}{b^2} = \frac{-6 \times 166.67}{2.5^2} = -160.0 \text{ t/m}^2$$

x/b y/b	Contribution of $\sigma_x$ Due to	0.00		0.25		0.50		0.75		1.00		1.25		1.50		1.75		2.00	
		Coeff	$\sigma_x$	Coeff	$\sigma_x$	Coeff	$\sigma_x$	Coeff	$\sigma_x$	Coeff	$\sigma_x$	Coeff	$\sigma_x$	Coeff	$\sigma_x$	Coeff	$\sigma_x$	Coeff	$\sigma_x$
0.00	Shear Force	0.00	0.00	0.6994	(-)13.988	2.925	(-)58.5	1.0246	(-)20.492	0.6994	(-)13.988	0.539 4	(-)10.788	0.441 3	(-)8.826	0.374 2	(-)7.484	0.325 2	(-)6.504
	Direct Load	1.00	28.8	1.00	28.8	1.00	28.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	Moment	0.0	0.0	0.50	(-)80.0	1.00	(-)160.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	Total		28.8		(-)65.188		(-)189.70		(-)20.492		(-)13.988		(-)10.788		(-)8.826		(-)7.484		(-)6.504
0.25	Shear Force	0.0	0.0	0.385	(-)7.7	0.602 3	(-)12.046	0.669 5	(-)13.35	0.582	(-)11.64	0.486 8	(-)9.736	0.413 1	(-)8.262	0.357 3	(-)7.146	0.314 2	(-)5.284
	Direct Load	0.450 2	12.965 8	0.392 9	11.316	0.347 1	9.996	0.285 1	8.211	0.170 7	4.916 2	0.108 2	3.116 1	0.074 1	2.134 1	0.053 9	1.552 3	0.040 9	1.177 9
	Moment	0.0	0.0	0.004	(-)0.64	0.046	(-)7.36	0.092 9	(-)14.864	0.0504	(-)8.064	0.027	(-)4.32	0.015 8	(-)2.528	0.01	(-)1.600	0.006 7	(-)1.072
	Total		12.965 8		2.975 5		(-)9.41		(-)20.000		(-)14.787 8		(-)10.94		(-)8.656		(-)7.193 7		(-)6.183 1
0.50	Shear Force	0.00	0.0	0.147 4	(-)2.948	0.257 7	(-)5.154	0.348 8	(-)6.976	0.385 0	(-)7.70	0.3 734	7.468	0.344 6	(-)6.892	0.313 4	(-)6.268	0.284 6	(-)5.60
	Direct Load	0.181 7	5.233 0	0.186 2	5.362 6	0.225 1	6.482 8	0.248 9	7.168 3	0.211 2	6.082 6	0.1 614	4.648 3	0.122 0	3.513 6	0.093 9	2.704	0.073 9	2.128 3
	Moment	0.000	0.0	(-)0.054 4	(+)8.704	(-)0.032 6	(+)5.216	0.024 5	(-)3.92	0.037 5	(-)6.0	0.0 301	(-)4.816	0.021 5	(-)3.44	0.015 2	(-)2.432	0.010 9	(-)1.744
	Total		5.233 0		11.118 6		6.544 8		(-)3.727 7		(-)7.617 4		(-)7.635 7		(-)6.818		(-)5.996		(-)5.125 7
0.75	Shear Force	0.00	0.0	0.0598	(-)11.96	0.121 5	(-)2.43	0.187 3	(-)3.746	0.238 5	(-)4.77	0.262 7	(-)5.254	0.265 7	(-)5.394	0.257 4	(-)5.148	0.244 2	(-)4.884
	Direct Load	0.080 5	2.318 4	0.097 8	28.166	0.142 4	4.101	0.180 6	5.201 3	0.184 8	5.322 2	0.165 0	4.752	0.138 8	3.997 4	0.114 5	3.297 6	0.094 5	2.721 6
	Moment	0.000	0.00	(-)0.040 8	(+)6.528	(-)0.039 8	(+)6.368	(-)0.010 0	(+)1.600	(-)0.011 9	(+)1.904	0.018 5	(-)2.96	0.017 7	(-)2.832	0.014 8	(-)2.368	0.011 8	(-)1.888
	Total		2.3184		22.734		8.039		3.055 3		2.456 2		(-)3.462		(-)4.228 6		(-)4.218 4		(-)4.050 4
1.00	Shear Force	0.00	0.0	0.026 9	(-)0.538	0.061 5	(-)1.23	0.104 9	(-)2.098	0.147 4	2.948	0.178 8	(-)3.576	0.196 2	(-)3.924	0.202 4	(-)4.048	0.201 4	(-)4.029
	Direct Load	0.040 5	1.166 4	0.055 1	1.586	0.090 8	2.615	0.126 9	3.654 7	0.145 7	4.196 2	0.145 6	4.193 2	0.134 2	3.864 9	0.118 8	3.241 4	0.103 2	2.972 1
	Moment	0.000	0.0	(-)0.026 2	(+)4.192 0	(-)0.032 1	5.136	(-)0.019 4	(+)3.104	(-)0.003 6	0.576	(-)0.006 4	(+)1.024	0.010 4	(-)1.664	0.011 0	(-)1.76	0.010 1	(-)1.616
	Total		1.166 4		5.24		6.521		4.660 7		1.824 2		1.641 2		(-)1.723 1		(-)2.386 6		(-)2.671 9
1.25	Shear Force	0.00	0.00	0.013 4	(-)0.268	0.033 2	(-)0.644	0.061 2	(-)1.224	0.092 7	(-)1.859	0.121	(-)2.420	0.142 0	(-)2.84	0.155 1	(-)3.102	0.161 6	(-)3.232
	Direct Load	0.022 7	0.653 7	0.033 2	0.956	0.059 5	1.713 6	0.089 2	2.568 9	0.111 0	3.968	0.120 4	3.467 5	0.119 6	3.444	0.112 6	3.242 8	0.102 8	2.960 6
	Moment	0.000	0.0	(-)0.016 8	(+)2.688	(-)0.023 6	(+)3.776	(-)0.019 3	3.088	(-)0.009 9	(+)1.584	(-)0.001 5	(+)0.24	0.003 8	(-)0.608	0.006 4	(-)1.024	0.007 2	(-)1.152
	Total		0.653 7		(+)3.376		4.825 6	(-)0.019 3	4.432 9		(-)0.241 2		1.287 5		(-)0.004		(-)0.883 1		(-)1.423
1.50	Shear Force	0.000	0.0	0.007 2	(-)0.144	0.019 1	(-)0.382	0.037 3	(-)0.746	0.059 8	(-)1.196	0.082 6	(-)1.651	0.102 4	(-)2.048	0.117 4	(-)2.348	0.127 5	(-)2.55
	Direct Load	0.013 8	0.397 4	0.021 2	0.610 5	0.040 3	1.160 6	0.063 6	1.831 6	0.083 9	2.416 3	0.096 9	2.790 7	0.102 1	2.94	0.101 3	2.917 4	0.096 7	2.784 9
	Moment	0.00	0.0	(-)0.011 1	(+)1.776	(-)0.017	(+)2.736	(-)0.0164	(+)2.624	(-)0.011 5	(+)1.84	(-)0.005 6	(+)0.896	(-)0.000 8	(+)0.128	0.002 4	(-)0.384	0.004 2	(-)0.672
	Total		0.397 4		(+)2.242 5		3.514 6		3.709 6		3.060 3		2.034 7		1.02		0.185 4		(-)0.437 1
1.75	Shear Force	0.000	0.0	0.004 2	(-)0.084	0.011 6	(-)0.232	0.023 6	(-)0.472	0.039 6	(-)0.792	0.057 2	1.144	0.074 1	(-)1.482	0.088 6	(-)1.772	0.099 8	(-)1.996
	Direct Load	0.009 0	2.592	0.014 2	0.408 9	0.028 1	0.809 2	0.046 3	1.333	0.063 8	1.837	0.077 2	2.223	0.085 3	2.456 6	0.088 4	2.545 9	0.087 8	2.528 6
	Moment	0.000	0.0	(-)0.007 6	1.216	(-)0.0124	(+)1.984	(-)0.013 3	(+)2.128	(-)0.010 9	(-)1.744	(-)0.007 2	(+)1.152	(-)0.003 4	(+)0.540	(-)0.000 4	(+)0.064	0.001 6	(-)0.256
	Total		2.592		1.540 9		2.561 2		2.989		2.789		2.231		1.518 6		0.837 9		0.276 6
2.00	Shear Force	0.000 0	0.000	0.002 6	(-)0.052	0.007 4	(-)0.148	0.015 5	(-)0.31	0.026 9	(-)0.538	0.040 3	(-)0.806	0.054 1	(-)1.082	0.067 0	(-)1.34	0.078	(-)1.56
	Direct Load	0.006 2	0.178 6	0.010 0	0.288	0.020 3	0.584 6	0.034 3	0.987 8	0.049 0	1.411 2	0.061 5	1.771 2	0.070 6	2.032 3	0.075 9	2.185 9	0.077 9	2.243 5
	Moment	0.000 0	0.00	(-)0.005 4	(+)0.864	(-)0.009 2	(+)1.472	(-)0.010 5	(-)1.68	(-)0.009 6	(+)1.536	(-)0.007 4	(+)1.184	(-)0.004 7	(+)0.752	(-)0.002 2	(-)0.352	0.000 2	0.032
	Total		0.178 6		1.100		1.908 6		2.357 8		2.409 2		2.149 2		1.702 3		1.197 9		0.715 5

Sign Convention : (-) = Tensile stresses.

(+) = Compressive stresses.



Table 8 Computation of Vertical Stress ( $\sigma_v$ ) at Different Points

(Annex A)

$$\frac{F}{b} = \frac{-50}{2.5} = -20.0 \text{ t/m}^2$$

$$\frac{P}{b} = \frac{72}{2.5} = 28.8 \text{ t/m}^2$$

$$\frac{6M}{b^2} = \frac{-6 \times 166.667}{2.5^2} = -160.0 \text{ t/m}^2$$

x/b y/b	Contribution of $\sigma_v$ Due to	0.00		0.25		0.50		0.75		1.00		1.25		1.50		1.75		2.00	
		Coeff	$\sigma_v$	Coeff	$\sigma_v$	Coeff	$\sigma_v$	Coeff	$\sigma_v$	Coeff	$\sigma_v$	Coeff	$\sigma_v$	Coeff	$\sigma_v$	Coeff	$\sigma_v$	Coeff	$\sigma_v$
0.00	Shear Force	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	Direct Load	1.00	28.8	1.00	28.80	1.00	28.8	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	Moment	0.00	0.00	(-0.500)	(-80.0)	1.00	(-160.0)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	Total		28.8		(-51.2)		(-131.2)				0.00		0.00		0.00		0.00		0.00
0.25	Shear Force	0.00	0.00	0.127 3	(-2.546)	0.299 6	(-5.992)	0.146 9	(-2.938)	0.0551	(-1.102)	0.025 5	(-0.51)	0.013 8	(-0.276)	0.008 4	(-0.168)	0.005 5	(-0.11)
	Direct Load	0.957 5	27.635	0.902 2	25.983 4	0.496 9	14.310 7	0.089 2	2.568 9	0.019 3	0.555 8	0.006 3	0.181 4	0.002 7	0.077 7	0.001 3	0.037 4	0.000 7	0.020 1
	Moment	0.000	0.00	0.387 5	(-62.00)	0.347 1	(-55.536)	0.060 4	(-9.664)	0.011 1	(-1.776)	0.003 1	(-0.496)	0.001 1	(-0.176)	0.000 5	(-0.08)	0.000 2	(-0.032)
	Total		27.635		(-38.562 6)		(-47.217 3)		(-10.033 1)		(-2.322 2)		(-0.824 6)		(-0.374 3)		(-0.210 6)		(-0.121 9)
0.50	Shear Force	0.00	0.00	0.156 7	(-3.134)	0.254 6	(-5.092)	0.210 7	(-4.214)	0.127 3	(-2.546)	0.073 9	(-1.478)	0.044 9	(-0.898)	0.028 9	(-0.578)	0.019 6	(-0.392)
	Direct Load	0.818 3	23.567 0	0.734 7	21.159 4	0.479 7	13.815 3	0.213 7	6.154 5	0.083 9	2.416 3	0.035 8	1.031	0.017 2	0.495 4	0.009 2	0.264 9	0.005 3	0.152 6
	Moment	0.00	0.00	0.210 6	(-33.696)	0.225 1	(-36.016)	0.109 9	(-17.584)	0.040 5	(-6.48)	0.015 5	(-2.48)	0.006 6	(-1.056)	0.003 1	(-0.496)	0.001 6	(-0.256)
	Total		23.567 0		(-15.670 6)		(-27.292 7)		(-15.643 5)		(-6.609 7)		(-2.927)		(-1.458 6)		(-0.809 1)		(-0.495 4)
0.75	Shear Force	0.00	0.00	0.127 3	(-2.546)	0.203 7	(-4.074)	0.202 2	(-4.044)	0.156 7	(-3.134)	0.109 8	(-2.196)	0.075 3	(-1.506)	0.052 4	(-1.048)	0.037 4	(-0.748)
	Direct Load	0.668 2	19.244 1	0.607 1	17.484 5	0.448 0	12.902 4	0.270 5	7.790 4	0.145 7	4.196 2	0.077 2	2.223 4	0.042 5	1.224	0.024 7	0.711 3	0.015 1	0.434 9
	Moment	0.00	0.00	0.112 5	(-18.0)	0.142 4	(-22.784)	0.102 4	(-16.384)	0.056 3	(-9.008)	0.028 4	(-4.544)	0.014 5	(-2.32)	0.007 7	(-1.232)	0.004 3	(-0.688)
	Total		19.244 1		(-3.061 5)		(-13.955 6)		(-12.637 6)		(-7.945 8)		(-4.516 6)		(-2.602)		(-1.568 7)		(-1.001 1)
1.00	Shear Force	0.00	0.00	0.095 9	(-1.918)	0.1592	(-3.184)	0.175 4	(-3.503)	0.1567	(-3.134)	0.1254	(-2.508)	0.095 5	(-1.91)	0.071 7	(-1.434)	0.034 0	(-1.08)
	Direct Load	0.549 8	15.834 2	0.510 5	14.702 4	0.409 2	11.784 9	0.287 6	8.282 9	0.184 8	5.322	0.114 2	3.288 9	0.070 6	2.033 3	0.044 5	1.281 6	0.028 9	0.832 3
	Moment	0.00	0.00	0.063 5	(-10.16)	0.090 8	(-14.528)	0.080 7	(-12.912)	0.056 3	(-9.008)	0.034 9	(-5.584)	0.020 8	(-3.328)	0.012 4	(-1.984)	0.007 5	(-1.20)
	Total		15.834 2		2.624 4		(-5.927 1)		(-8.137 1)		6.820		(-4.803 3)		(-3.204 7)		(-2.136 4)		(-1.447 7)
1.25	Shear Force	0.00	0.00	0.072 0	(-1.44)	0.124 2	(-2.484)	0.146 9	(-2.938)	0.144 0	(-2.88)	0.126 5	(-2.53)	0.104 7	(-2.09 4)	0.084 1	(-1.682)	0.066 8	(-1.336)
	Direct Load	0.461 8	13.299 8	0.436 5	12.398 4	0.370 0	10.656	0.285 1	8.210 8	0.204 5	5.889 6	0.140 7	4.052 2	0.095 2	2.711 8	0.064 6	1.860 5	0.044 3	1.275 8
	Moment	0.00	0.00	0.038 7	(-6.112)	0.059 5	(-9.52)	0.060 4	(-9.664)	0.049 2	(-7.872)	0.035 4	(-5.664)	0.023 9	(-3.824)	0.015 8	(-2.528)	0.010 4	(-1.664)
	Total		13.299 8		4.846 4		(-1.348)		(-4.391 2)		(-4.862 4)		(-4.141 8)		(-3.376 2)		(-2.349 5)		(-1.724 2)
1.50	Shear Force	0.00	0.00	0.055 1	(-1.102)	0.097 9	(-1.958)	0.121 9	(-2.438)	0.127 3	(-2.546)	0.119 8	(-2.396)	0.105 8	(-2.116)	0.089 9	(-1.798)	0.074 9	(-1.498)
	Direct Load	0.395 8	11.399 0	0.379 1	10.918 1	0.334 1	9.622 1	0.273 5	7.876 8	0.211 2	6.082 6	0.156 8	4.515 8	0.113 9	3.280 3	0.082 1	2.361 5	0.059 3	1.707 8
	Moment	0.00	0.00	0.024 4	(-3.900)	0.040 3	(-6.443)	0.049 7	(-7.152)	0.040 5	(-6.48)	0.032 5	(-5.20)	0.024 3	(-3.888)	0.017 5	(-2.80)	0.012 3	(-1.968)
	Total		11.399 0		5.912 1		1.221 1		(-1.713 2)		(-2.943 4)		(-3.080 2)		(-2.723 7)		(-2.236 5)		(-1.758 2)
1.75	Shear Force	0.00	0.00	0.043 0	(-0.86)	0.078 4	(-1.568)	0.101 2	(-2.024)	0.110 8	(-2.216)	0.109 8	(-2.196)	0.101 9	(-2.038)	0.090 8	(-1.816)	0.078 8	(-1.576)
	Direct Load	0.345 3	9.949 6	0.333 9	9.616 3	0.302 4	8.709 1	0.258 3	7.439	0.210 2	6.053 8	0.165 0	4.752	0.126 6	3.646 1	0.095 9	2.761 9	0.072 3	2.082 2
	Moment	0.00	0.00	0.016 3	(-2.608)	0.028 1	(-4.496)	0.033 3	(-5.328)	0.032 6	(-5.216)	0.028 4	(-4.544)	0.023 0	(-3.668)	0.017 7	(-2.832)	0.013 3	(-2.128)
	Total		9.949 6		6.148 3		2.645 1		0.087		(-1.378 2)		(-1.988 0)		(-2.071 9)		(-1.886 1)		(-1.621 8)
2.00	Shear Force	0.00	0.00	0.034 3	(-0.686)	0.637	(-12.74)	0.084 5	(-1.69)	0.095 9	(-1.918)	0.098 8	(-1.976)	0.095 5	(-1.910)	0.088 4	(-1.768)	0.079 5	(-1.590)
	Direct Load	0.305 8	8.807 0	0.297 6	8.570 9	0.214 9	7.917 1	0.242 1	6.972 8	0.204 7	5.895 4	0.167 7	4.829 8	0.342	3.864 9	0.105 9	3.049 9	0.082 9	2.387 5
	Moment	0.00	0.00	0.011 4	(-1.824)	0.020 3	(-3.248)	0.025 1	(-4.016)	0.026	(-4.160)	0.024 1	(-3.856)	0.020 8	(-3.328)	0.017 0	(-2.720)	0.013 5	(-2.16)
	Total		8.807 0		6.060 9		(-8.070 9)		1.266 5		(-0.182 6)		(-1.002 2)		(-1.1373 1)		(-1.438 1)		1.362 5

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